

Computational Intelligence

Lecture 8: Designing Controller Using Neural Networks

Farzaneh Abdollahi

Department of Electrical Engineering

Amirkabir University of Technology

Open-Loop Inverse Dynamics

NN in Control Feedback

Gradient Through Plant

Gradient Through The Model of The Plant

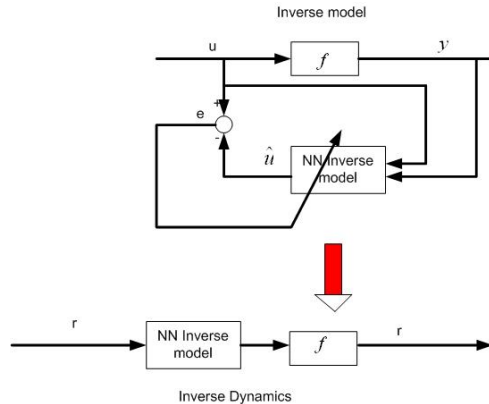
Adaptive Control Using Neural Networks

Open-Loop Inverse Dynamics

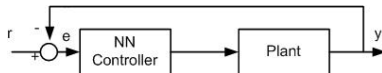
- ▶ The Inverse model obtained from identification is directly applied.
- ▶ \therefore Considering reference signal r

$$y = f^{-1}fr = r$$

- ▶ This method can be considered as Indirect adaptive control



NN in Control Feedback



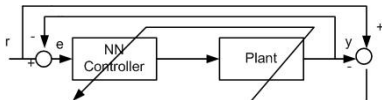
- ▶ **Objective:** Tracking reference signal r
- ▶ **But:** In this model, output of NN for training is not available \rightsquigarrow BP can not be applied directly.

$$e = r - y, \quad E = \frac{1}{2}e^2$$

$$\Delta w_{ij} = -\eta \frac{\partial E}{\partial w_{ij}}$$

- ▶ Only output of the plant, y is available.

Gradient Through Plant



- ▶ The plant can be considered as output layer of NN with fixed weights
- ▶ \therefore desired output of the NN is available and BP algorithm can be employed.

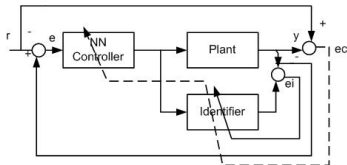
$$\frac{\partial E}{\partial w_{ij}} = \frac{\partial E}{\partial e} \cdot \frac{\partial e}{\partial y} \cdot \frac{\partial y}{\partial w_{ij}}$$

$$\frac{\partial E}{\partial e} = e, \quad \frac{\partial e}{\partial y} = -1$$

$$\frac{\partial y}{\partial w_{ij}} = \frac{\partial y}{\partial u} \cdot \frac{\partial u}{\partial w_{ij}}$$

- ▶ To train the NN, $\frac{\partial y}{\partial u}$ is required, therefore, this method is so-called **Gradient through plant**

NN in Control Feedback

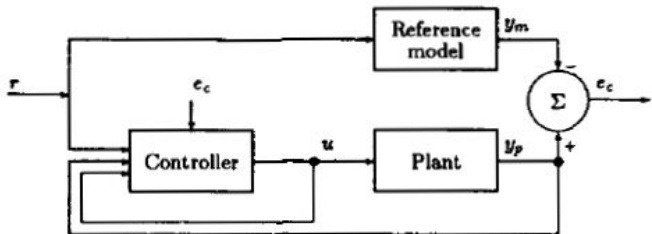


- ▶ If the plant dynamics is not known $\frac{\partial y}{\partial u}$ is not available!!
- ▶ Solution
 1. Using a NN identifier to identify the system dynamics directly.
 - ▶ Then apply $\frac{\partial \hat{y}}{\partial u}$ instead of $\frac{\partial y}{\partial u}$.
 - ▶ This method is so-called **Gradient Through The Model of The Plant**
 2. Approximate $\frac{\partial y}{\partial u}$ with $\text{sign}\left\{\frac{\partial y}{\partial u}\right\}$ which is usually available without knowing the dynamics
 - ▶ If the direction of the gradient is true, the magnitude of $\frac{\partial y}{\partial u}$ can be compensated by η

Adaptive Control Using Neural Networks

1. Direct Control

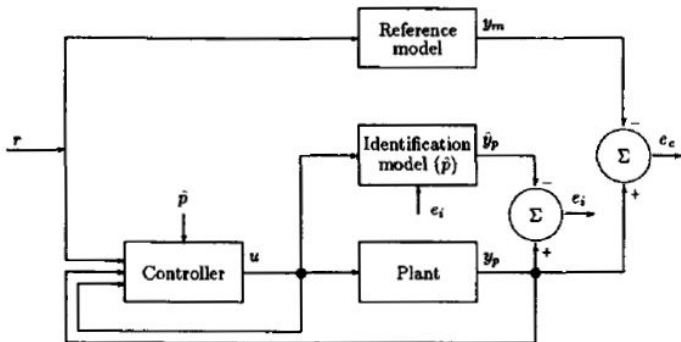
- Parameters of the controller is directly adjusted to reduce the norm of output error



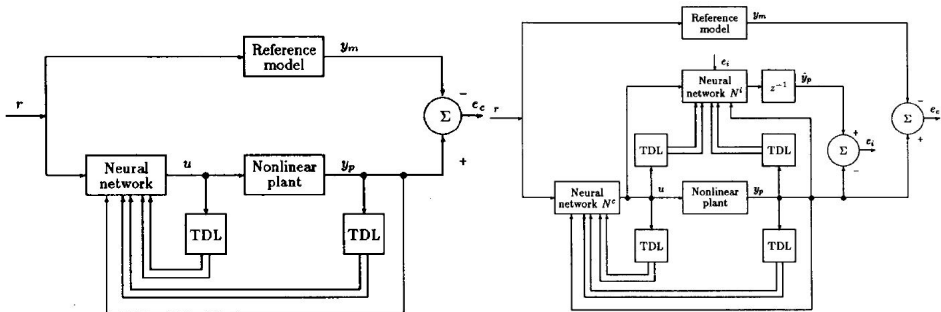
Adaptive Control Using Neural Networks

2. Indirect Control

- ▶ The model of the plant is identified first and the parameters of the controller is defined based on identified model



- ▶ They can be a neural networks controller



Example [1]

- ▶ Consider the difference equation:

$$y_p(k+1) = f[y_p(k), y_p(k-1)] + u(k)$$

- ▶ $f(\cdot)$ is unknown

- ▶ For the sake of simulation $f[y_p(k), y_p(k-1)] = \frac{y_p(k)y_p(k-1)[y_p(k)+2.5]}{1+y_p^2(k)+y_p^2(k-1)}$

- ▶ Reference model: $y_m(k+1) = 0.6y_m(k) + 0.2y_m(k-1) + r(k)$

- ▶ $r(k) = \sin(\frac{2\pi k}{25})$: a bounded reference input

- ▶ **Objective:** Determine a bound control signal $u(k)$ s.t.

$$\lim_{k \rightarrow \infty} e_c(k) = y_p(k) - y_m(k) = 0$$

Example Cont'd

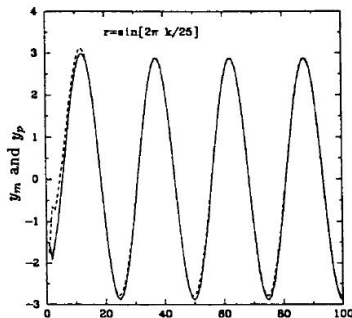
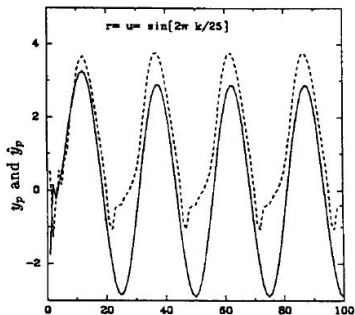
- ▶ If $f(\cdot)$ was known the proper control signal would be $u(k) = -f[y_p(k), y_p(k-1)] + 0.6y_p(k) + 0.2y_p(k-1) + r(k)$ yields $e_c(k+1) = 0.6e_c(k) + 0.2e_c(k-1)$
 - ▶ \therefore the reference model is a.s. since $\lim_{k \rightarrow \infty} e_c(k) = 0$
- ▶ Since the plant is unknown, assuming the unforced system is stable, $f(\cdot)$ is estimated by series parallel NN identifier as $\hat{f}(\cdot)$
- ▶ Hence $u(k) = -\hat{f}[y_p(k), y_p(k-1)] + 0.6y_p(k) + 0.2y_p(k-1) + r(k)$

Example Cont'd

- ▶ Identification will be off-line
- ▶ Once the plant is identified in desired level of accuracy, control is initiated to make the plant output follow the reference model.
- ▶ **Note that** using the estimated function in fb loop may result in unbounded solution
- ▶ Hence for on-line control, identification and control should proceed simultaneously.
- ▶ The time interval T_i and T_c for updating the identification and control parameters should be chosen wisely.

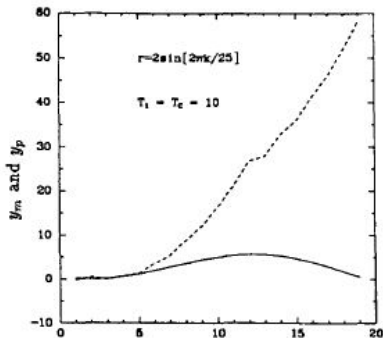
Example Cont'd

- ▶ a) Identified signal \hat{y}_p (dashed) and output of the plant with no control action (solid)
- ▶ b) Response for $r = \sin(\frac{2\pi k}{25})$ with control (dashed); reference signal (solid)
- ▶ $T_i = T_c = 1$



Example Cont'd

- ▶ Choose $T_i = T_c = 10$
- ▶ Response for $r = \sin\left(\frac{2\pi k}{25}\right)$ with control (dashed); reference signal (solid)
- ▶ \therefore To have stable on-line control, the identification should be accurate enough before the control action is initiated!



Example 2 [1]

- ▶ Consider the difference equation:

$$y_p(k+1) = f[y_p(k), y_p(k-1), \dots, y_p(k-n+1)] + \sum_{j=0}^{m-1} \beta_j u(k-j) \quad m \leq n$$

- ▶ $f(\cdot)$ and β_j are unknown; β_0 is nonzero with known sign

- ▶ For the sake of simulation

$$f[y_p(k), y_p(k-1), \dots, y_p(k-n+1)] = \frac{5y_p(k)y_p(k-1)}{1+y_p^2(k)+y_p^2(k-1)+y_p^2(k-2)};$$

$$\beta_0 = 1, \beta_1 = 0.8$$

- ▶ Reference model:

$$y_m(k+1) = 0.32y_m(k) + 0.64y_m(k-1) - 0.5y_m(k-2) + r(k)$$

- ▶ $r(k) = \sin(\frac{2\pi k}{25})$: a bounded reference input

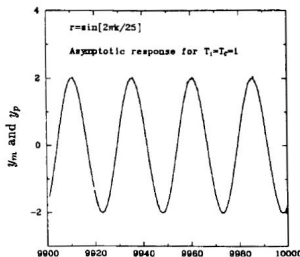
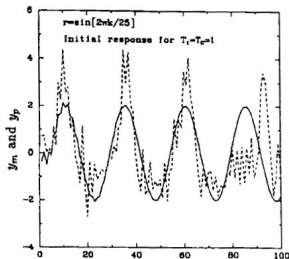
- ▶ **Objective:** Determine a bound control signal $u(k)$ s.t.

$$\lim_{k \rightarrow \infty} e_c(k) = y_p(k) - y_m(k) = 0$$

- ▶ Assume $\text{sgn}(\beta_0) = +1$; $\beta_0 \geq 0.1$

Example 2 Cont'd

- ▶ The control signal is: $u(k) = \frac{1}{\hat{\beta}_0} [-\hat{f}_k[y_p(k), y_p(k-1), y_p(k-2)] - \hat{\beta}_1 u(k-1) + 0.32y_p(k) + 0.64y_p(k-1) - 0.5y_p(k-2) + r(k)]$
- ▶ Choose $T_i = T_c = 10$
- ▶ Response for $r = \sin(\frac{2\pi k}{25})$ with control (dashed); reference signal (solid) left): first 100 sec; right) after 9900sec

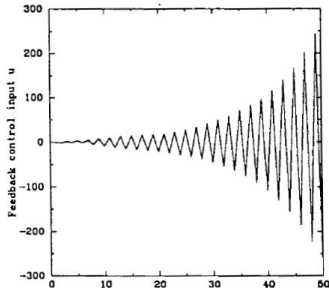
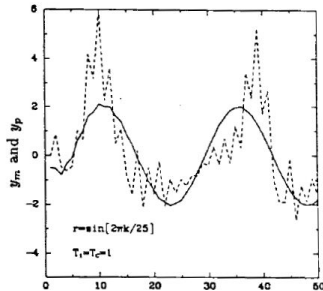


Example 3 [1]

- ▶ Consider dynamics similar to Example 2 but replace $0.8u(k-1)$ with $1.1u(k-1)$
- ▶ Apply similar controller
- ▶ The system is nonminimum phase (it has zero out of unit circle)
- ▶ \therefore The output error is bounded but the control signal is unbounded

Example 3 Cont'd

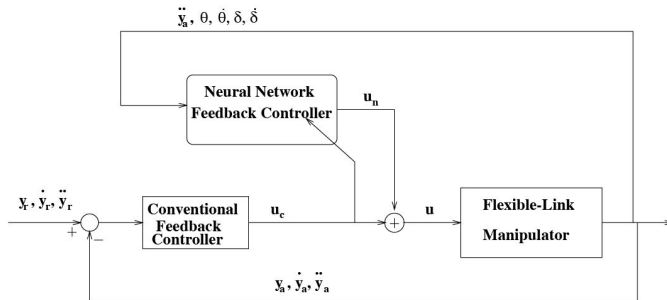
- ▶ left) Response for $r = \sin(\frac{2\pi k}{25})$ with control (dashed); reference signal (solid)
- ▶ right) control signal $u(k)$



Inverse Dynamics Model Learning (IDML) [2]

- ▶ Consider the system dynamics $\ddot{x} = f(x, \dot{x}) + u$, $y = x$
- ▶ To track reference signal y_a , control signal can be defined $u = u_n + u_c$
 - ▶ $u_c = (-\ddot{y}_a) + K_1(\dot{y}_r - \dot{y}_a) + K_0(y_r - y_a)$ is conventional FB controller
 - ▶ $u_n = -f(x, \dot{x})$
- ▶ $f(\cdot)$ is not known and is estimated by NN $\rightsquigarrow u_n = \hat{f}$

- ▶ The error signal for training is $e_n = u - u_n = u_c$
- ▶ The learning rule is $\dot{w} = \eta \frac{\partial \hat{f}}{\partial w} u_c$



Example 4 [2]

- ▶ Consider one-link flexible arm:

$$M(\delta) \begin{bmatrix} \ddot{\theta} \\ \ddot{\delta} \end{bmatrix} + \begin{bmatrix} h_1(\dot{\theta}, \delta, \dot{\delta}) + F_1 \dot{\theta} + f_c \\ h_2(\dot{\theta}, \delta) + K\delta + F_2 \dot{\delta} \end{bmatrix} = \begin{bmatrix} u \\ 0 \end{bmatrix}$$

- ▶ θ : hub angle
- ▶ δ : deflection variable
- ▶ h_1 and h_2 are Coriolis and Centrifugal forces, respectively
- ▶ $M(\delta)$: P.D. inertia matrix
- ▶ u : torque
- ▶ F_1 : viscous damping; F_2 damping matrix;
- ▶ f_c hub friction; K stiffness matrix

Example 4 Cont'd

- ▶ The nonlinear dynamics is assumed to be unknown
- ▶ For the sake of simulation, the numerical values are

$$\text{▶ } M(\delta) = \begin{bmatrix} m(\delta) & 1.0703 & -0.0282 \\ 1.0703 & 1.6235 & -0.4241 \\ -0.0282 & -0.4241 & 2.592 \end{bmatrix};$$

$$m(\delta) = 0.9929 + 0.12(\delta_1^2 + \delta_2^2) - 0.24\delta_1\delta_2$$

$$\text{▶ } K = \begin{bmatrix} 17.4561 & 0 \\ 0 & 685.5706 \end{bmatrix}$$

$$\text{▶ } h_1(\dot{\theta}, \delta, \dot{\delta}) = 0.24\dot{\theta}[(\delta_1 - \delta_2)\dot{\delta}_1 - (\delta_1 - \delta_2)\dot{\delta}_2]$$

$$\text{▶ } h_2(\dot{\theta}, \delta) = \begin{bmatrix} -0.12\dot{\theta}^2(\delta_1 - \delta_2) \\ -0.12\dot{\theta}^2(\delta_2 - \delta_1) \end{bmatrix}$$

$$\text{▶ } f_c = C_{coul}\left(\frac{2}{1+e^{-10\dot{\theta}}} - 1\right); C_{coul} = \begin{cases} 4.74 & \dot{\theta} > 0 \\ 4.77 & \dot{\theta} < 0 \end{cases}$$

- ▶ By output redefinition, the nonminimum phase problem is solved

Example 4 Cont'd

- ▶ The NN structure:
 - ▶ Three layer: 4 input; 5 hidden, 1 output
- ▶ $K_0 = 1; K_1 = 2$

Example 4 Cont'd

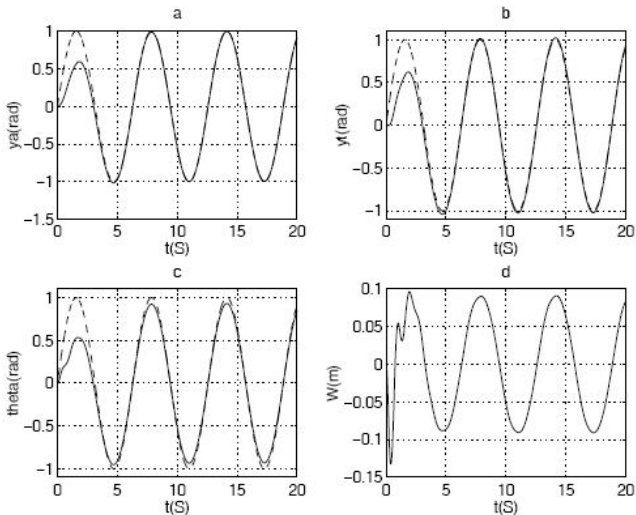


Figure 4.7: Output responses for System II to $\sin(t)$ reference trajectory using the Neural Networks

Example 4 Cont'd

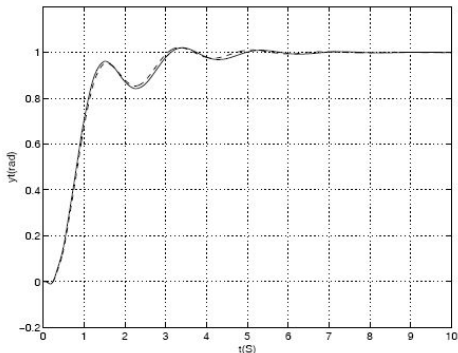


Figure 4.8: Actual tip responses to step input for System II using the IDML neural network controller; (dashed line corresponds to model with Coulomb friction at the tip).

References



K. S. Narendra and K. Parthasarathy, "Identification and control of dynamical systems using neural networks," *IEEE Trans. on Neural Networks*, vol. 1, no. 1, pp. 4–27, March 1990.



H.A. Talebi, .R.V Patel and K. Khorasani, *Control of Flexible-link Manipulators Using Neural Networks*.
Springer, 2001.